

# Cu–Mn–Ce ternary mixed-oxide catalysts for catalytic combustion of toluene

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#### ARTICLE INFO

Article history: Received 30 August 2014 Revised 28 October 2014 Accepted 13 November 2014 Available online 24 April 2015

Keywords: Cu–Mn–Ce mixed oxide Toluene Catalytic combustion Volatile organic compounds (VOCs)

#### ABSTRACT

Cu–Mn, Cu–Mn–Ce, and Cu–Ce mixed-oxide catalysts were prepared by a citric acid sol–gel method and then characterized by XRD, BET, H<sub>2</sub>-TPR and XPS analyses. Their catalytic properties were investigated in the toluene combustion reaction. Results showed that the Cu–Mn–Ce ternary mixed-oxide catalyst with 1:2:4 mole ratios had the highest catalytic activity, and 99% toluene conversion was achieved at temperatures below 220°C. In the Cu–Mn–Ce catalyst, a portion of Cu and Mn species entered into the CeO<sub>2</sub> fluorite lattice, which led to the formation of a ceria-based solid solution. Excess Cu and Mn oxides existed on the surface of the ceria-based solid solution. The coexistence of Cu–Mn mixed oxides and the ceria-based solid solution resulted in a better synergetic interaction than the Cu–Mn and Cu–Ce catalysts, which promoted catalyst reducibility, increased oxygen mobility, and enhanced the formation of a bundant active oxygen species.

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# Introduction

Volatile organic compounds (VOCs) are some of the most harmful air pollutants because they are acutely toxic toward the environment and humans (Parmar and Rao, 2009). Among various available techniques, catalytic combustion is an effective and widely applied technology for the abatement of VOCs (Everaert and Baeyens, 2004). The low operating temperature and high efficiency of this technology has led to considerable environmental and economic benefits, as well as application in the field of industrial emission (Huang et al., 2008; Lu et al., 2011). The catalysts most commonly used in the combustion of VOCs are of two types, namely, those based on noble metals and metal mixed oxides. Noble metal catalysts are widely used in the catalytic combustion of VOCs (Okumura et al., 2003; Saqer et al., 2009). However, in addition to the high cost of noble metal catalysts, they are susceptible to poisons such as impurities in the feed stream or intermediates formed during oxidation (Zhao et al., 2010). Thus, intensive efforts are being directed toward the design and synthesis of catalytic materials based on metal oxides as a substitute for noble metal catalysts (Lu et al., 2013a, 2013b). Manganese and copper mixed oxides are considered highly active and promising catalysts for the combustion of VOCs (Morales et al., 2006; Zimowska et al., 2007). Morales et al. (2006) prepared stable crystalline-phase mixed MnO<sub>X</sub> and CuO catalysts by coprecipitation, and investigated their performance in ethanol and propane catalytic combustion. They found that the catalyst activity was generally as good as that of noble metal catalysts, such as those based on platinum and palladium (Du et al., 2008; Morales et al., 2009).

The CuMn<sub>2</sub>O<sub>4</sub> spinel oxide structure is considered the main active phase in Cu–Mn catalysts. However, the CuMn<sub>2</sub>O<sub>4</sub> structure easily decomposes into Cu<sub>x</sub>Mn<sub>3 - x</sub>O<sub>4</sub> ( $\chi$  = 1.4–1.6)

http://dx.doi.org/10.1016/j.jes.2014.11.015

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and  $Mn_2O_3$  or  $Mn_3O_4$  at high temperature (Tanaka et al., 2005). In a sense,  $Cu_{1.5}Mn_{1.5}O_4$  is the real active phase. Hutchings et al. (1998) also proved that the  $Cu_{1.5}Mn_{1.5}O_4$  and  $MnO_{\chi}$  mixed structure is the main active site in Cu-Mn composite oxide catalysts during CO oxidation. Even in the methanol steam-reforming reaction, Papavasiliou et al. (2006, 2007) also considered that  $Cu_{\chi}Mn_{3-\chi}O_4$  spinel oxide and  $MnO_{\chi}$  are the main active phases. In summary, the presence of such a mixed structure of  $Cu_{1.5}Mn_{1.5}O_4$  and  $MnO_{\chi}$  plays an important role in the catalytic oxidation of VOCs over Cu-Mn-based catalysts.  $Cu_{1.5}Mn_{1.5}O_4$  is the active site, whereas  $MnO_{\chi}$  is the center of oxygen supply and transmission for providing  $Cu_{1.5}Mn_{1.5}O_4$  with active oxygen to completely oxidize organic molecules.

Based on the abovementioned active structure model, we believe that if other metal oxides with better oxygen-supply capacity and oxygen storage capacity are used to replace  $MnO_x$ , the activity of Cu–Mn catalysts can be further promoted.  $CeO_2$  is known to have excellent oxygen storage capacity and is widely used in the field of catalytic oxidation (Wang et al., 2008; Lu et al., 2013a). Therefore, using Ce as a partial substitute for Mn in Cu–Mn catalysts can enable the preparation of catalysts with better oxygen capacity and higher performance for the catalytic oxidation of toluene.

In the present work, a series of Cu, Mn, and Ce mixed oxides with different Cu/Mn/Ce ratios was prepared and characterized by X-ray diffraction (XRD), Brunauer–Emmett–Teller (BET), H<sub>2</sub>-temperature programmed reduction (TPR), and X-ray photoelectron spectroscopy (XPS) analyses. Their catalytic activities were evaluated in the catalytic combustion of toluene. The reaction mechanisms and structural features of these mixed-oxide catalysts were also discussed.

#### 1. Experimental

#### 1.1. Catalyst preparation

Mixed-oxide catalysts were prepared by a citric acid sol-gel method with appropriate amounts of Cu, Mn, and Ce nitrates as precursors. Copper nitrate, manganese nitrate, and cerium nitrate were mixed in appropriate molar ratios in an appropriate volume of distilled water to obtain a transparent solution (1.0 mol/L metal ion concentration). Then citric acid equimolar to the metal nitrates was added to the nitrate solution. The resulting solution was stirred and dried at 110°C overnight to form a solid gel. This gel was then calcined at 500°C for 3 hr. The obtained samples were ground, pelletized, and sieved to between 20 and 30 mesh size. The synthesized catalysts are hereafter denoted as  $Cu_xMn_yCe_z$ , where x:y:z represents the different Cu:Mn:Ce molar ratios. For comparison, samples of CuO,  $MnO_x$ , and  $CeO_2$  were also prepared by the same method.

#### 1.2. Catalyst characterization

## 1.2.1. BET specific surface area

The specific surface area of the catalysts was measured by the BET method from nitrogen adsorption isotherms. Experiments

were carried out on a Micromeritics ASAP 2020 instrument at 77 K. Prior to experiments, samples were degassed at 427 K for 3 hr.

#### 1.2.2. X-ray diffraction (XRD)

XRD data of the samples were collected on a SCINTAG XTRA X-ray diffractometer equipped with Ni-filtered Cu K $\alpha$  ( $\lambda$  = 1.542 Å, 40 kV) radiation. The measurements were conducted within the 2 $\theta$  range of 10°–60° with a step size of 0.033°.

#### 1.2.3. Temperature programmed reduction (TPR)

TPR experiments were performed on a Autochem 3010E (Zhejiang Fine-Tech Instruments, China). A desired amount of sample (200 mg) was placed in a quartz reactor, pretreated in a flow of Ar gas at 250°C for 2 hr, and cooled to 70°C. A gas mixture of  $H_2$  (5%) and Ar (95%) was then passed (30 mL/min) through the reactor. The temperature was increased from 70°C to 750°C at a heating rate of 10°C/min. A TCD detector was used at the outlet of the reactor to measure the volume of hydrogen consumed during reduction.

#### 1.2.4. X-ray photoelectron spectroscopy (XPS)

A Kratos AXIS Ultra DLD photoelectron spectrometer with a monochromatized microfocused Al X-ray source was used for XPS measurements (Shimadzu scientific instruments, Japan). The charging of samples was corrected by setting the binding energy of adventitious carbon (C 1s) at 284.6 eV. Prior to measurements, the powdered samples were pressed into self-supporting disks, loaded into a sub-chamber, and then evacuated at 25°C for 4 hr.

#### 1.3. Catalytic activity measurement

Catalytic combustion of toluene was conducted in a fixed-bed quartz tube reactor (10 mm i.d.) at atmospheric pressure. About 500 mg of catalyst mixed 1.5 g quartz sand was packed at the isothermal zone of the reactor. Gaseous VOCs were generated by flowing air from a mass-flow controller through liquid organics in an incubator placed in an ice bath. The VOC-containing stream was mixed with the main air stream introduced through another mass-flow controller. The feed (5.0 g/m<sup>3</sup> toluene in air) was introduced to the catalyst at a flow rate of 200 mL/min (gas hourly space velocity = 24,000 mL/(hr(gcat.))). The reactor effluent was analyzed online at desired temperatures with an HP 6890 gas chromatography system equipped with a flame ionization detector.

# 2. Results and discussions

#### 2.1. Activity test

Morales et al. (2006) and Papavasiliou et al. (2007) confirmed that interactions among Cu–Mn oxides promote the activation of lattice oxygen, decrease the light-off temperature, and increase the dispersion of the active species. The selectivity to  $CO_2$  also increases with increased Mn proportion. Many studies (Zimowska et al., 2007; Du et al., 2008; Morales et al., 2008) have shown that  $Cu_{\chi}Mn_{1-\chi}$  ( $\chi = 0.1$ –0.3) catalysts



Fig. 1 – Light-off curves of toluene combustion over Cu–Mn–Ce mixed-oxide catalysts. Conditions: GHSV = 24,000 mL/(hr(gcat.)), toluene concentration: 5 g/m<sup>3</sup>.

possess excellent catalytic performance, especially for the combustion of oxygen-containing organic compounds (*e.g.*, ethyl acetate, ethanol, acetone, *etc.*). These catalysts show strong oxidation ability, high selectivity toward  $CO_2$ , and even better catalytic performance than noble metals. Therefore,  $Cu_1Mn_6$  was used in the current research as a Cu-Mn mixed-oxide catalyst model, and on this basis, Ce was used to partially substitute for Mn.

Fig. 1 shows the light-off curves of toluene combustion over Cu–Mn, Cu–Mn–Ce, and Cu–Ce catalysts. The activity of Cu–Mn–Ce ternary mixed-oxide catalysts is higher than those of Cu–Mn and Cu–Ce mixed-oxide catalysts. The performance of pure oxides (CuO, CeO<sub>2</sub>, and MnO<sub> $\chi$ </sub>) in the total oxidation of toluene is lower than those of the mixed oxides. Complete toluene combustion occurs at 320°C over MnO<sub> $\chi$ </sub> catalysts, and 99% toluene combustion occurs at 270°C over the Cu<sub>1</sub>Mn<sub>6</sub> catalyst. With the partial substitution of Mn by Ce, the activity of Cu–Mn–Ce catalysts is promoted, and the conversion curves shift to a much lower temperature. Both Cu<sub>1</sub>Mn<sub>4</sub>Ce<sub>2</sub> and Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> appear to be superior for toluene catalytic combustion, which reaches 99.0% conversion when the reaction proceeds at about 230 and 220°C, respectively. This



Fig. 2 –  $T_{50}$  and  $T_{90}$  of Gu–Mn–Ce ternary mixed-oxide catalysts for toluene combustion.

result is similar to those for conventional noble metal catalysts, such as Pd (Schwartz and Pfefferle, 2012) and Pt (Saqer et al., 2009). The experimental results in Fig. 2 indicate that  $T_{50}$  and  $T_{90}$  (where 50% and 90% conversions are reached) gradually decrease with Ce/(Cu + Mn + Ce) ratio from 0 to 0.57. However, the catalytic activity declines when Ce completely replaces Mn. This indicates that Mn ion is an essential element in the catalyst active phase during toluene combustion.

#### 2.2. Texture characterization of catalysts

To gain a deep insight into the structural evolution, XRD patterns of the catalysts were measured and are shown in Fig. 3. The diffraction peaks of the Cu<sub>1</sub>Mn<sub>6</sub> catalyst mainly correspond to the Cu<sub>15</sub>Mn<sub>15</sub>O<sub>4</sub> and Mn<sub>3</sub>O<sub>4</sub> phases, which is different from catalysts prepared by coprecipitation (mainly Mn<sub>2</sub>O<sub>3</sub> crystal phase) (Morales et al., 2008). The XRD patterns of  $Cu_1Mn_2Ce_4$  and  $Cu_1Ce_6$  catalysts show a single  $CeO_2$  phase. No Cu and Mn oxide phases are found in the XRD patterns of the catalysts, indicating that a ceria-based solid solution structure is formed by the doping of Cu and Mn ions. Comparison of the XRD patterns of pure CeO<sub>2</sub> and Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> catalysts reveals a decrease in the lattice parameter of Cu-Mn–Ce catalysts. In the Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> sample, the cell constant declines from 0.5410 to 0.5364 nm, indicating that ceria-based solid solutions are formed by partial replacement of Ce<sup>4+</sup> with these transition metal cations. Because the Mn<sup>4+</sup>, Mn<sup>3+</sup>, Cu<sup>2+</sup>, and Cu<sup>+</sup> ionic radii are 0.056, 0.062, 0.073, and 0.077 nm, respectively, which are all less than that of Ce<sup>4+</sup> (0.097 nm), the lattice constant decreases on substitution.

Liang et al. (2008) and Tang et al. (2008) proved that when the Ce content is more than 50% in Cu–Ce and Mn–Ce catalysts, a solid solution of CeO<sub>2</sub> is easily formed. However, a solubility limit for Cu and Mn cations in CeO<sub>2</sub> was reported by Aranda et al. (2012) and Kang et al. (2006). The limit of Cu doping in the CeO<sub>2</sub> lattice is less than 14%, and that of Mn is about 5 mol% to 10 mol%, and highly depends on the preparation procedure. In the Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> catalyst, the Cu and Mn contents are 14.3 mol% and 28.6 mol%, respectively.



Fig. 3 – XRD patterns of CeO<sub>2</sub>,  $Cu_1Mn_6$ ,  $Cu_1Ce_6$  and  $Cu_1Mn_2Ce_4$  mixed-oxide catalysts.

Table 1 – Crystal structure and specific surface area of catalysts.						
Samples	BET surface (m²/g)	XLBA size (nm)	Cell (CeO <sub>2</sub> ) (a/nm)	Reduction temperature (°C)		H <sub>2</sub> consumption (mmol/g)
				T <sub>1</sub>	T <sub>2</sub>	
Cu <sub>1</sub> Mn <sub>6</sub>	37.9	12.5	/	200	280	5.72
$Cu_1Mn_2Ce_4$	45.3	5.80	0.5364	180	/	2.32
Cu <sub>1</sub> Ce <sub>6</sub>	68.3	7.30	0.5400	150	/	1.93
CeO <sub>2</sub>	62.0	10.2	0.5410	520	/	2.66

Excess Cu and Mn in the Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> catalysts may be highly dispersed on the surface of CeO<sub>2</sub> as CuO<sub> $\chi$ </sub>, MnO<sub> $\chi$ </sub>, or their mixed oxides. The crystalline structure, particle size, and morphology of the catalysts were also investigated by TEM. The high-resolution TEM image of the Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> catalyst is presented in Fig. 4. Several lattice fringes of the crystal structures of Cu and Mn oxides (lattice fringes = 0.253 and 0.187 nm) besides that of CeO<sub>2</sub> (lattice fringes = 0.312 nm) are observed. Therefore, the high activity of the Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> catalyst can be reasonably attributed to its double active structures. One is a mixed structure of Cu and Mn oxides with the function of activating organic molecules. The other one is a ceria-based solid solution structure with the function of transporting active oxygen, including surface and lattice oxygen.

Moreover, the BET surface areas of the catalysts are also listed in Table 1. The surface area of  $Cu_1Mn_2Ce_4$  is 45.3 m<sup>2</sup>/g, which is higher than that of  $Cu_1Mn_6$  (37.9 m<sup>2</sup>/g). However, compared with pure CeO<sub>2</sub> catalyst, the crystallinity of  $Cu_1Mn_2Ce_4$  decreases and the average grain size becomes the smallest. This finding indicates that the presence of Cu and Mn in the lattice of CeO<sub>2</sub> results in change to the original phase of the CeO<sub>2</sub> crystalline structure, thereby leading to decreased crystallinity.

# 2.3. H<sub>2</sub>-TPR characterization

Results of TPR analyses for the catalysts are shown in Fig. 5.  $Cu_1Mn_6$  reduction occurs in the form of two peaks at 230°C

and 280°C. The peak at a low temperature can be assigned to the reduction of  $Cu_{1.5}Mn_{1.5}O_4$ ; the other one is a shoulder peak associated with the reduction of  $Mn_3O_4$ , which can be related to the presence of the  $Mn_3O_4$  and Mn ions with valence lower than +3. When some Mn ions are replaced by Ce, the reduction peaks shift to considerably lower temperatures compared with the  $Cu_1Mn_6$  catalyst. Specifically, the main reduction peaks of  $Cu_1Mn_2Ce_4$  and  $Cu_1Ce_6$  sharply shift to 180 and 150°C from 230°C, respectively.

The two reduction peaks of pure CuO normally appear at around 200°C. However, for pure MnO<sub>v</sub>, a small reduction peak can be observed at 380°C, which is assigned to the reduction of Mn<sub>3</sub>O<sub>4</sub> to MnO (Dai et al., 2012). MnO<sub>y</sub> doped with an amount of CuO can effectively promote the reduction of  $\text{MnO}_{\scriptscriptstyle X}$  , which may be due to two effects: First, CuO has a strong ability of activating the H-H bond, a function common to precious metals. With active H ion overflow occurring,  $MnO_{\chi}$  reduction occurs. Second, the crystallinity of  $MnO_{\chi}$ decreases.  $MnO_{\chi}$  forms lattice defects and oxygen vacancies as a result of CuO doping, which results in enhanced mobility of active oxygen. Morales et al. (2008) milled CuO and Mn<sub>2</sub>O<sub>3</sub> to form a mechanical mixed-solid compound and found that CuO does not change the reduction performance of  $MnO_{y}$ . However, after high-temperature calcination, CuO and MnO<sub>v</sub> form a new crystalline phase that results in decreased reduction temperature and increased catalytic activity. Therefore, only the interaction between CuO and Mn forming a new crystalline phase can effectively improve their



Fig. 4 – HRTEM image of Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> ternary mixed-oxide catalysts.



Fig. 5 –  $H_2$ -TPR of CeO<sub>2</sub>, Cu<sub>1</sub>Mn<sub>6</sub>, Cu<sub>1</sub>Ce<sub>6</sub> and Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> mixed-oxide catalysts.

catalytic oxidation. The second mechanism of lattice defects in Cu–Mn mixed oxides is widely accepted by current researchers.

Considering that Ce is partially substituted for Mn in the catalysts, Cu and Mn ions in the crystalline phase of CeO<sub>2</sub> lead to decreased crystallinity, creating more lattice defects and oxygen vacancies that favor increased oxygen mobility. In addition, the reduction peak of the Cu–Mn–Ce catalyst occurs at lower temperatures compared with the Cu–Mn catalyst, thereby confirming that the defects in the ceria-based solid solution have better oxygen capacity. In addition, The H<sub>2</sub>-consumption of the catalysts is listed in Table 1. The H<sub>2</sub>-consumption of Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> is 2.32 mmol/g, which is higher than that of Cu<sub>1</sub>Ce<sub>6</sub> (1.93 mmol/g); and the H<sub>2</sub>-consumption of the Cu<sub>1</sub>Mn<sub>6</sub> catalysts is the highest. We propose that the H<sub>2</sub>-consumption during reduction directly relates to the oxygen capacity of the catalyst. Namely, the increase of Mn valence is the key factor responsible for the increase of H<sub>2</sub>-consumption.

# 2.4. XPS characterization

The reactive oxygen species located in the mixed-oxide catalysts were characterized by XPS, and the results are shown in Fig. 6. The  $O_{1s}$  XPS spectra can be resolved into three peaks (Tang et al., 2006): (1) lattice oxygen ( $O_{latt}$ ) at 529 to 530 eV; (2) surface oxygen ( $O_{sur}$ ) at 530 to 532 eV, which is assigned to defect oxides or surface oxygen ions with low coordination and weakly bonded oxygen species; and (3) adsorbed oxygen species ( $O_{ads}$ ) at 533 to 534 eV from hydroxyl species and adsorbed water species as contaminants on the surface. The peak from 530 to 532 eV corresponds to surface-adsorbed oxygen.

Fig. 6 shows that an increase in the amount of Ce as a substitute for Mn causes an  $O_{1S}$  shift to a higher binding energy. The binding energy is 530.9 eV for  $Cu_1Mn_6$  and shifts to 531.6 eV for  $Cu_1Mn_2Ce_4$ . This result indicates that surface oxygen increases with increased amounts of Ce in the catalysts. Bielanski and Haber (1979) proposed three types of lattice oxygen on the catalyst surface:  $O_2^{2-}$ ,  $O^-$ , and  $O^{2-}$ .  $O_2^{2-}$  and



Fig. 6 – XPS spectra of  $O_{1S}$  of CeO<sub>2</sub>, Cu<sub>1</sub>Mn<sub>6</sub>, Cu<sub>1</sub>Ce<sub>6</sub> and Cu<sub>1</sub>Mn<sub>2</sub>Ce<sub>4</sub> mixed-oxide catalysts.

 $O^-$  are electrophilic oxygen species (surface oxygen) that readily participate in excessive and complete oxidation, whereas nucleophilic oxygen species such as  $O^{2^-}$  (lattice oxygen) mainly play an important role in selective oxidation. The XPS results reveal that the substitution of Ce for Mn in Cu-Mn catalysts can increase the number of electrophilic surface oxygen atoms, thereby effectively promoting the activity for total oxidation.

For  $Cu_{\chi}Mn_{1-\chi}$  ( $\chi$  = 0.1–0.3) catalysts, the activity improvement was attributed to the presence of the  $Cu_{1.5}Mn_{1.5}O_4$  mixed phase and a poorly crystalline manganese oxide, possessing a large amount of oxygen vacancies and lattice defects, which not only create more active oxygen, but also provide the transport channels for active oxygen.  $Cu_{1.5}Mn_{1.5}O_4$  serves as the actual active phase and has excellent oxidation capabilities. Crystalline-phase  $Mn_3O_4$  is the center of oxygen supply, with better reducing properties. Based on this theory, the substitution of Ce for Mn in the Cu–Mn catalyst can strongly enhance its redox capabilities. To further improve this catalytic activity, the underlying mechanism was confirmed in our experiment.

For Cu-Mn-Ce ternary oxide catalysts, the formation of a ceria-based solid solution and Cu-Mn oxide active phase with the function of activating organic molecules is the critical factor affecting catalytic combustion at low temperatures. When Ce is partially substituted for Mn, Cu and Mn enter the fluorite-like lattice, leading to the formation of a ceria-based solid solution. Active structures of CeO2-based solid solutions mainly depend on abundant oxygen vacancies, good oxygen transmission, and increased reduction capability. The CeO2-based solid solution serves as the oxygen-supplying center with the function of transporting active oxygen, including surface and lattice oxygen. In addition, excess Cu and Mn in Cu-Mn-Ce catalysts are highly dispersed on the surface of CeO<sub>2</sub> as an active phase of Cu-Mn mixed oxides, which has a strong ability to activate organic molecules, thereby serving as the catalyst oxidation center. Therefore, high activity can be reasonably achieved over the  $Cu_1Mn_2Ce_4$  catalyst.

# 3. Conclusions

The partial substitution of Mn by Ce in Cu–Mn catalysts induces a significant change in the structure of the Cu–Mn mixed oxide catalysts. A new ceria-based solid solution phase with the fluorite structure forms, and excess Cu and Mn exist on the surface of the ceria-based solid solution. The CeO<sub>2</sub>-based solid solution serves as the oxygen-supplying center with the function of transporting active oxygen, including surface and lattice oxygen. In addition, Cu–Mn mixed oxides are highly dispersed on the surface of CeO<sub>2</sub> as an active phase and can strongly activate organic molecules, thereby serving as the catalyst oxidation center. The resulting structure is highly active for the catalytic combustion of VOCs.

#### Acknowledgments

We would like to acknowledge the financial support from the Natural Science Foundation of China (No. 21107096), Zhejiang Provincial Natural Science Foundation of China (No. Y14E080008), the Commission of Science and Technology of Zhejiang province (No. 2013C03021), and the Specialized Research Fund for the Doctoral Program of Higher Education (No. 20133317110004).

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