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# A facile route for spraying preparation of  $Pt/TiO<sub>2</sub>$  monolithic catalysts toward VOCs combustion



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environmental friendliness, and high utilization of active components.

### 1. Introduction

The rapid development of industries led to a significant increase in volatile organic compounds (VOCs) emissions [\[1,](#page-8-0)[2\]](#page-8-1). In addition to their toxicity, VOCs exposed to ultraviolet light in the atmosphere can cause ozone pollution and even photochemical smog pollution, which seriously harm the environment and human health [\[3](#page-8-2)–7]. The control of VOCs aroused tremendous attention. An increasing number of researchers are committed to eliminating VOCs.

Among the relevant techniques [8–[12](#page-8-3)], such as adsorption, thermal incineration, photocatalytic degradation, plasma-catalytic oxidation, and catalytic combustion, catalytic combustion is a widely used technology for removing VOCs due to its advantages of less energy consumption, high treatment efficiency, absence of secondary pollution, and good environmental and economic benefits [\[13](#page-8-4)–18]. The most commonly used combustion catalysts are noble metal catalysts and complex metal oxides catalysts. Noble metal catalysts, which have superior catalytic activity, selectivity and universality, are the main catalysts in practical application. Pt-based materials are considered the most ideal catalyst for catalytic combustion [19–[23\]](#page-8-5). He et al. prepared Pt/TiO<sub>2</sub> catalyst through impregnation method using anatase TiO<sub>2</sub> as support; they found that formaldehyde could be completely oxidized over the catalyst at room temperature [[24\]](#page-8-6). Peng et al. synthesized Pt/ HPMOR through impregnation method, wherein the  $T_{90}$  of toluene combustion was 190°C [\[25](#page-8-7)]. Santos et al. reported noble metal catalysts supported on  $TiO<sub>2</sub>$  by liquid-phase reduction deposition were active for the total oxidation of CO and VOCs [\[26](#page-8-8)].

However, the catalysts most widely used to treat industrial waste gases are monolithic ones because they offer great advantages over grained catalysts, such as improved mechanical properties and mass/ heat transfer [[27\]](#page-8-9). The preparation of monolithic catalysts presently involves the following steps. The washcoat is coated on the surface of the structured monolithic substrate followed by loading of active species through impregnation. Alternatively, the slurry prepared from powder catalyst is directly coated on the surface of the structured monolithic substrate, and the monolithic catalyst is obtained through activation treatment. The preparation process is cumbersome and the active components are easily lost, thereby leading to poor utilization ratio and increased preparation cost. Moreover, the active component in the prepared monolithic catalyst shows poor dispersion and adhesive strength, which seriously affect the activity and stability of the monolith catalyst [\[28](#page-8-10)]. Therefore, existing studies focus on reducing cost and

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energy consumption and improving the efficiency of the monolithic catalysts in practical applications. A simple and efficient preparation strategy for monolithic catalysts must be adopted [[29\]](#page-8-11).

We reported a facile strategy for preparing monolithic catalysts through spraying method [\[30](#page-8-12)[,31](#page-8-13)]. The present strategy focuses on the following points: preparing the nanoparticle (NP) dispersion liquid with catalytic activity for combustion through solvothermal method and spraying the dispersion liquid on the different substrates to obtain monolith catalysts. This strategy simplifies the preparation process of monolithic catalysts and improves the utilization of active components. Moreover, this strategy can reactivate catalysts when deactivated through respraying without replacing the monolithic catalysts. This process greatly minimizes hazardous waste generation and the costs of preparation and operation. In this study, active nano-Pt/TiO<sub>2</sub> dispersion liquid was synthesized through hydrolysis and chemical reduction method which is simpler and greener. The physical and chemical properties of Pt/TiO<sub>2</sub> NPs were characterized. And various Pt/TiO<sub>2</sub> monolithic catalysts were successfully prepared via simply spraying the dispersion liquid.

### 2. Experimental

#### 2.1. Chemical agents

Tetrabutyl titanate  $(C_{16}H_{36}O_4Ti;TBT, CP)$  and acetic acid (CH<sub>3</sub>COOH, AR) were purchased from Shanghai Lingfeng Chemical Reagent Co., Ltd. Chloroplatinic acid hexahydrate (H<sub>2</sub>PtCl<sub>6</sub>·6H<sub>2</sub>O, AR) was purchased from Aladdin. Ethyl alcohol absolute (CH<sub>3</sub>CH<sub>2</sub>OH, AR) was purchased from Anhui Ante Food Co., Ltd. Hydrazine hydrate (N2H4·H2O 85%, AR) was purchased from Sinopharm Chemical Reagent Co., Ltd. P25 was purchased from Degussa AG. Polyethylene glycol (HO (CH2CH2O)nH; PEG8000, AR) was purchased from Shanghai Macklin Biochemical Co., Ltd. Toluene  $(C_7H_8$ , AR) was purchased from Quzhou Juhua Reagent Co., Ltd.

### 2.2. Catalyst preparation

The nano-Pt/TiO<sub>2</sub> dispersion liquid and monolithic catalysts were prepared as follows (Fig. S1). The nano-Pt/TiO<sub>2</sub> dispersion liquid was synthesized via hydrolysis and chemical reduction. TBT (3.5 mL) was added to the mixed solution (30 mL of ethanol, 10 mL of acetic acid and 10 mL of deionized water) under stirring. The solution reacted by stirring at 40 °C for 5 h. The H<sub>2</sub>PtCl<sub>6</sub> solution (2 mmol·L $^{-1}$ ; 0 mL, 2 mL, 10 mL) was added to the cooled homogeneous clear solution. The hydrazine hydrate solution (compound at once when using, 24 mmol $\rm L^{-1};$ 0 mL, 0.5 mL, 2.5 mL) was added by dropping during stirring. The resulting solution was diluted to 40 mL to obtain nano-Pt/TiO<sub>2</sub> dispersion liquid (20 mg mL<sup>-1</sup>) after reacting at room temperature for 12 h. According to the mass ratio (0 wt%, 0.1 wt%, 0.5 wt%) of Pt to TiO<sub>2</sub>, the Pt/TiO<sub>2</sub> dispersion liquids were denoted by TiO<sub>2</sub>, 0.1 Pt/TiO<sub>2</sub>, and  $0.5$  Pt/TiO<sub>2</sub>.

Pt/TiO2 powder catalysts were obtained via drying or calcination. The Pt/TiO<sub>2</sub> dispersion liquids dried at 110 °C were denoted by TiO<sub>2</sub>-d, 0.1 Pt/TiO<sub>2</sub>-d, and 0.5 Pt/TiO<sub>2</sub>-d. These catalysts calcined at 400 °C for 3 h under air were denoted by TiO<sub>2</sub>-c, 0.1 Pt/TiO<sub>2</sub>-c, and 0.5 Pt/TiO<sub>2</sub>-c.

Pt/TiO<sub>2</sub> monolithic catalysts were obtained through dispersion-liquid-spraying method. The  $0.5$  Pt/TiO<sub>2</sub> dispersion liquids (8 mL) were sprayed onto cordierite honeycomb ( $\Phi$  1.5 cm, h 5 cm, ~8 g). The resulting cordierite honeycomb (the mass ratio of  $Pt/TiO<sub>2</sub>$  to cordierite honeycomb: 2 wt%) dried at 110 °C was denoted by  $0.5 \, \text{Pt/TiO}_2/\text{CH}$ (the mass ratio of Pt to cordierite honeycomb: 0.1 wt‰). This catalyst was calcined at 400 °C for 3 h under air and was denoted by 0.5 Pt/  $TiO<sub>2</sub>/CH-c$ . The other Pt/TiO<sub>2</sub> monolithic catalysts (the mass ratio of Pt/TiO<sub>2</sub> to support: 2 wt%) were prepared by spraying a certain amount of  $0.5$  Pt/TiO<sub>2</sub> on reticulated SiC, foamed alumina, and brick. They were denoted as  $0.5 \text{ Pt/TiO}_2/\text{SiC}$ ,  $0.5 \text{Pt/TiO}_2/\text{Al}_2\text{O}_3$ , and  $0.5 \text{Pt/TiO}_2/\text{Al}_2\text{O}_3$ 

Brick. The catalysts calcined at 400 °C for 3 h under air were denoted by 0.5 Pt/TiO<sub>2</sub>/SiC-c, 0.5 Pt/TiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>-c, and 0.5 Pt/TiO<sub>2</sub>/Brick-c.

R-Pt/TiO<sub>2</sub> monolithic catalysts were prepared through slurrycoating method. Certain amounts of P25 and polyethylene glycol (the mass ratio of PEG to P25: 1 wt%) were added to deionized water through stirring. The mixture was stirred at room temperature for 6 h to form TiO<sub>2</sub> slurry (0.02 g/mL). The cordierite honeycomb was impregnated with the slurry for 30 min and then dried at 110 °C for 5 h. This process was repeated three times. The  $TiO<sub>2</sub>$ -coated cordierite honeycomb was calcined at 400 °C for 3 h under air. The content of TiO<sub>2</sub> on cordierite honeycomb was approximately 2 wt%. H<sub>2</sub>PtCl<sub>6</sub> solution (3 mL, 2 mmol·L<sup>-1</sup>) was diluted to 40 mL, and the TiO<sub>2</sub>-coated cordierite honeycomb fully immersed into it for  $24$  h. The Pt/TiO<sub>2</sub>coated cordierite honeycomb dried at 110 °C was denoted by R-0.5 Pt/ TiO<sub>2</sub>/CH (the mass ratio of Pt/TiO<sub>2</sub> to support: 2 wt%). This catalyst was calcined at 400 °C for 3 h under air and was denoted by R-0.5 Pt/ TiO<sub>2</sub>/CH-c.

## 2.3. Catalyst characterization

A Tecnai F30 S-Twin transmission electron microscope operated at 300 kV was used for transmission electron microscopy (TEM). Samples for TEM investigation were prepared by dropping  $Pt/TiO<sub>2</sub>$  dispersion liquid onto a carbon-coated copper grid.

X-ray diffraction (XRD) patterns were recorded on a PANalytical X' Pert PRO diffractometer instrument operated at 40 kV and 30 mA, with Cu Kα-ray radiation ( $\lambda = 1.54178$  Å). Scans were taken with a 2θ range from 10° to 80°.

Scanning electron microscopy (SEM) images were obtained on a Hitachi S-4700(II) microscope operated at 15.0 kV.

N2 adsorption-desorption isotherms of the samples were carried out at 77 K on a Micromeritics ASAP2020 instrument. The specific surface areas and the mesopore sizes of the samples were calculated using the Brunauer-Emmett-Teller (BET) and Barrett-Joyner-Halenda (BJH) method, respectively. All samples were pre-treated in vacuum at 200 °C for 5 h before measurements.

 $H<sub>2</sub>$  temperature-programmed reduction ( $H<sub>2</sub>-TPR$ ) was measured on a FINE SORB-3010 E instrument equipped with a thermal conductivity detector (TCD). The sample was placed in a quartz reactor, pre-treated in Ar flow at 200 °C for 1 h and cooled down at 50 °C. The catalyst bed was performed by admitting a flow of 5 vol%  $H<sub>2</sub>/Ar$  at 60 °C for 10 min, followed by heating at a constant rate  $(10 °C min^{-1})$  up to 750 °C. Finally, the catalyst was cooled under the Ar flow. The flow rates in the experiment were 30 mL·min<sup>-1</sup>. Hydrogen consumption was monitored using TCD operated at 60 °C and 60 mA.

Adhesion test was conducted by immersing the monolithic catalyst after calcination in deionized water inside a beaker and vibrating in an ultrasonic vibration instrument (40 kHz/100 w) for 10, 30, and 60 min. The sample was then dried at 110 °C, and a catalytic performance test for toluene combustion was performed. Mass loss was calculated according to the following equation:

Mass  $loss = (M_0-M_1)/M_0 \times 100\%$ 

where  $M_0$  and  $M_1$  are the masses of the sample before and after ultrasonic vibration [[32\]](#page-8-14).

CO oxidation reaction was conducted in a fixed-bed microreactor. The powder catalyst was placed in a quartz reactor. Feed gas was 1 vol % CO balanced with air, and the gas flow rate was 40 mL min−<sup>1</sup> . The CO concentrations were detected by a gas chromatograph equipped with TCD. The conversion of CO was obtained on the basis of CO consumption and calculated by the inlet and outlet concentrations of CO. The turnover frequency (TOF) value of CO oxidation calculated on the basis of dispersion of Pt NPs on the catalyst surface and the conversion rate of CO as

$$
TOF = X_{CO} \cdot F_{CO} \cdot M_{Pt} / (m_{cat} \cdot X_{Pt} \cdot D_{Pt})
$$

where  $X_{\text{CO}}$  is the conversion rate of CO,  $F_{\text{CO}}$  is the flow rate of CO (mol h<sup>-1</sup>),  $m_{\text{cat}}$  is the mass of catalyst,  $X_{\text{Pt}}$  is the Pt content of catalyst,  $D_{\text{Pt}}$  is the dispersion of Pt (Table S1), and  $M_{\text{Pt}}$  is the molar mass of Pt.

#### 2.4. Catalytic activity test

The combustion of toluene activity over these catalysts was evaluated with a continuous flow-fixed bed reactor. The feed consists of 2000 ppm toluene was generated by bubbling standard air through a bottle that contained pure toluene placed in an ice-water mixture (0 °C). The gas hourly space velocity (GHSV) was 3000 h<sup>-1</sup> for cordierite honeycomb monolithic catalyst. The weight hourly space velocity (WHSV) was 34,000 mL  $g^{-1}$  h<sup>-1</sup> for powder catalyst. For other monolithic catalysts, WHSV was 370,000 mL g<sup>-1</sup> h<sup>-1</sup> (based on the Pt/TiO<sub>2</sub> of the load). The concentrations of the toluene were detected by a gas chromatograph equipped with FID. The conversion of toluene was obtained on the basis of the inlet and outlet concentrations of toluene. The TOF value of toluene combustion was calculated similar to that of CO oxidation.

## 3. Results and discussion

## 3.1. Characterization of  $Pt/TiO<sub>2</sub>$  dispersion liquid and NPs

# 3.1.1. Dispersion and phase analysis of Pt/TiO2 dispersion liquid

The dispersion and phase analysis of  $Pt/TiO<sub>2</sub>$  dispersion liquid are shown in [Figs. 1 and 2.](#page-2-0) [Fig. 1a](#page-2-0)-1, b-1 and c-1 show the photos of all Pt/  $TiO<sub>2</sub>$  dispersion liquid. Obviously, all samples were uniformly transparent, which indicated that the NPs were highly dispersed in liquid. The color of dispersion liquid deepened with the increase in Pt addition, which implied that Pt was successfully reduced and highly dispersed in the system. The crystal structure of the particles in the liquid was

verified by X-ray diffractometer. The results are shown in [Fig. 2](#page-3-0). The anatase  $TiO<sub>2</sub>$  with good crystallinity could be obtained by hydrolization of TBT. No characteristic peaks of Pt were observed in  $0.1$  Pt/TiO<sub>2</sub>-d and  $0.5$  Pt/TiO<sub>2</sub>-d ([Fig. 2a](#page-3-0)). The samples after calcination also just ex-hibited diffraction peaks of anatase TiO<sub>2</sub> ([Fig. 2b](#page-3-0)). The relatively small amount of the Pt in a highly dispersed form on the  $TiO<sub>2</sub>$  surface caused difficulty in XRD detection [\[33](#page-8-15)[,34](#page-8-16)].

TEM was used to evaluate the dispersion state and the bonding form of the  $Pt/TiO<sub>2</sub>$  in the liquid. The TEM images ([Figs. 1a](#page-2-0)-2–4, b-2–4 and c-2–4) show that the dispersion liquid would form a film on the surface of the substrate after drying. This formation is due to the fact that organics, such as acetic acid, are present in the dispersion liquid, and the  $TiO<sub>2</sub>$  NPs are connected to one another by the chelation of acetate when the concentration is high. TiO<sub>2</sub> NPs could be easily dispersed by dilution (Figs. S8a-1-3, b-1-3 and c-1-3), which indicated that the  $TiO<sub>2</sub> NPs$ prepared by this scheme were dispersed in the solution without reunion. Pt was introduced into the  $TiO<sub>2</sub>$  dispersion liquid by reduction of chloroplatinic acid using hydrazine hydrate as reducing agent. It could be observed that Pt NPs were dispersed on the surface of the  $TiO<sub>2</sub> film$ from TEM images of  $0.5 \text{Pt/TiO}_2$  ([Figs. 1c](#page-2-0)-2–4 and S8c-1–3), but the presence of Pt was difficult to observe from TEM images of 0.1 Pt/TiO<sub>2</sub> ([Figs. 1b](#page-2-0)-2–4 and S8b-1–4). However, the high-angle annular dark-field (HAADF)-TEM images (Fig. S9) illustrate that the smaller Pt NPs homodispersed on the surface of the TiO<sub>2</sub> film in 0.1 Pt/TiO<sub>2</sub>. [Table 1](#page-3-1) lists the size and dispersion of Pt in  $0.1$  Pt/TiO<sub>2</sub> (2.5 nm, 45.2%) and  $0.5$  Pt/TiO<sub>2</sub> (27.6 nm, 4.1%) calculated from HAADF-TEM images. This phenomenon was due to Pt NPs aggregation growth as the amounts of chloroplatinic acid and hydrazine hydrate increased. In addition, observing the TEM and HAADF-TEM images of Pt-containing samples ([Figs. 1b](#page-2-0)-2–4, c-2–4 and S8b-1–3, c-1–3), all Pt NPs appeared on the surface of TiO<sub>2</sub>, which indicated that Pt was already combined with  $TiO<sub>2</sub>$  in the dispersion liquid. [Fig. 1](#page-2-0)c-4 depicts that Pt NPs were

<span id="page-2-0"></span>

Fig. 1. The photos of TiO2 (a-1), 0.1 Pt/TiO2 (b-1) and 0.5 Pt/TiO2 (c-1); TEM images of TiO2 (a-2∼4), 0.1 Pt/TiO2 (b-2∼4) and 0.5 Pt/TiO2 (c-2∼4).

<span id="page-3-0"></span>

Fig. 2. XRD patterns of  $Pt/TiO<sub>2</sub>$  nanoparticles (a. uncalcined, b. calcined).

<span id="page-3-1"></span>Table 1 The dispersion of Pt.

The dispersion of Ft.		
Sample	d(nm)	$D(\%)$
$0.1$ Pt/TiO <sub>2</sub> $0.5 \, \text{Pt/TiO}_2$	2.5 27.6	45.2 4.1

supported on (101) plane of  $TiO<sub>2</sub>$ . Hence, the NPs in the dispersion were in the form of Pt on the surface of  $TiO<sub>2</sub>$ . The above characterization showed that the  $Pt/TiO<sub>2</sub>$  NP dispersion liquid can be easily obtained by the preparation strategy shown in Fig. S1a. An active film with active components uniformly dispersed on the substrate can be formed after spraying.

## 3.1.2. Textural properties of Pt/TiO2 NPs

The  $N_2$  adsorption-desorption technique was adopted to evaluate the texture structure of  $Pt/TiO<sub>2</sub>$  NPs. [Table 2](#page-3-2) lists some information about textural parameters of the samples derived from  $N_2$  adsorptiondesorption. It could been found that the samples after calcination showed increased pore size and decreased pore volume and  $S<sub>BET</sub>$ . This characterization was due to the pores with narrow necks and wide bodies (Fig. S10a), which originated from the aggregation of primary  $TiO<sub>2</sub>$  particles and the influence of organic matter, formed uniform and orderly cylindrical mesopores (Fig. S10c) when the organic matter was removed and the order degree increased with sample calcining. For calcined samples, the pore size, pore volume and  $S<sub>BET</sub>$  decreased with the increase in Pt loading amount. This phenomenon can be elucidated as follows. First, the density of the samples increased with increasing Pt loading because of the higher density of Pt (21.45  $\rm g\,cm^{-3})$  than that of TiO<sub>2</sub> (3.84 g·cm<sup>-3</sup>) given that the pore volume (cm<sup>3</sup>g<sup>-1</sup>) and S<sub>BET</sub>  $\rm (cm^2\,g^{-1})$  expressed per gram of the sample. Second, Pt was perfectly dispersed on the surface of  $TiO<sub>2</sub>$  and partially blocked the mesopores, thereby resulting in decreased in pore size, pore volume and  $S<sub>BET</sub>$  [\[35](#page-8-17)]. For uncalcined samples, the sequence of the pore size, pore volume, and  $S_{\text{BET}}$  is 0.1 Pt/TiO<sub>2</sub>-d > 0.5 Pt/TiO<sub>2</sub>-d > TiO<sub>2</sub>-d. This phenomenon can be

<span id="page-3-2"></span>Table 2





d: NPs obtained by drying; c: NPs obtained by calcination.

understood as follows. First, gas will be generated when hydrazine hydrate was added, which was obviously observed in preparation. Thus, the pore size, pore volume, and  $S<sub>BET</sub>$  increased due to poremaking ability of gas. Second, pore size, pore volume, and  $S<sub>BET</sub>$  decreased with the increase in Pt loading. Thus, the pore size, pore volume, and  $S<sub>BET</sub>$  of 0.5 Pt/TiO<sub>2</sub>-d slightly reduced than that of 0.1 Pt/  $TiO<sub>2</sub>-d$ .

In summary, the as-prepared  $Pt/TiO<sub>2</sub>$  NPs have good mesoporous structure (Fig. S10) and Pt dispersion, which is beneficial for the diffusion of the reactants and products. The activity must be improved, particularly for the relatively large molecules, such as toluene [[36\]](#page-8-18).

# 3.1.3. Chemical properties of  $Pt/TiO<sub>2</sub> NPs$

 $H_2$ -TPR was employed to investigate the redox capability of Pt/TiO<sub>2</sub> NPs, which is an important factor that affects catalytic reaction. [Fig. 3](#page-4-0) shows the H<sub>2</sub>-TPR profiles of all Pt/TiO<sub>2</sub> NPs. For the TiO<sub>2</sub>-d [\(Fig. 3](#page-4-0)a), the negative H<sub>2</sub>-consumption peaks at approximately 280 °C and 458 °C could be attributed to the influence of organic matter. The temperatures of these negative  $H_2$ -consumption peaks were relative to weight loss temperature of organic on the sample (Fig. S11a). The  $H_2$ -consumption peak at approximately 342 °C might be caused by the reaction of organics and hydrogen. For instance, the hydrogenation of acetate induced hydrogen consumption (Fig. S11b) [\[37](#page-8-19)]. However, the negative H2-consumption peak disappeared, and the trend of hydrogen consumption appeared at approximately 280 °C of 0.1 Pt/TiO<sub>2</sub>-d and  $0.5$  Pt/TiO<sub>2</sub>-d [\(Fig. 3](#page-4-0)a). This result was attributed to hydrogen spillover because of Pt. Another negative  $H_2$ -consumption peak at approximately 426 °C of 0.1 Pt/TiO<sub>2</sub>-d and 0.5 Pt/TiO<sub>2</sub>-d was due to back spillover. The H<sub>2</sub>-TPR curves of 0.1 Pt/TiO<sub>2</sub>-d and 0.5 Pt/TiO<sub>2</sub>-d were approximately the same. Thus, they exhibited the similar redox capability, which explained similar CO oxidation and toluene combustion activity over these two Pt/TiO<sub>2</sub> NPs [\(Figs. 4a](#page-4-1) and [5](#page-5-0) a).

The  $H_2$ -TPR curves of Pt/TiO<sub>2</sub> NPs after calcination are shown in [Fig. 3](#page-4-0)b. The intrinsic redox capability of  $Pt/TiO<sub>2</sub>$  NPs was given with the removal of organics. Reduction peak was not observed on the  $TiO<sub>2</sub>$ -c before 500 °C. H<sub>2</sub> consumption peaks at  $T > 500$  °C were attributed to the reduction of bulk oxygen of TiO<sub>2</sub> [[24\]](#page-8-6). The  $0.1$  Pt/TiO<sub>2</sub>-c sample showed three H<sub>2</sub>-consumption peaks before 500 °C. The H<sub>2</sub>-consumption peak at approximately 148 °C was associated to the reduction of PtO<sub>x</sub> crystallites to metallic Pt. Peak at approximately 290 °C could be attributed to hydrogen spillover because of Pt. The peak at approximately 432 °C might be caused by the reduction of the surface capping oxygen of TiO<sub>2</sub> [[38,](#page-8-20)[39](#page-8-21)]. These three reduction peaks also increased with increasing of Pt. For example, the two  $H_2$ -consumption peaks of 0.5 Pt/TiO<sub>2</sub>-c between 200 °C and 500 °C formed a maximum reduction peak, which greatly enhanced the reduction of oxygen species on  $TiO<sub>2</sub>$ 

<span id="page-4-0"></span>

Fig. 3. H<sub>2</sub>-TPR profiles of Pt/TiO<sub>2</sub> nanoparticles (a. uncalcined, b. calcined).

surface.

These results suggested that the as-prepared  $Pt/TiO<sub>2</sub>$  nanoparticles have good redox capability, which is beneficial for heterogeneous catalytic oxidation reactions [[40\]](#page-8-22).

CO oxidation is a structure-sensitive reaction and the reaction process is relatively simple. It is often used as the probe reaction to study the catalytic oxidation properties of catalysts in the scientific research field [\[41](#page-8-23)]. The light-off curves of CO oxidation are shown in [Fig. 4](#page-4-1)a to understand the chemical properties of the as-prepared  $Pt/TiO<sub>2</sub>$  NPs. The CO oxidation activity over TiO<sub>2</sub>-d was better than that of TiO<sub>2</sub>-c. This result could be attributed to the agglomeration of  $TiO<sub>2</sub>$  NPs during calcination and indicated that the as-prepared NPs in dispersion liquid were highly dispersed and had certain catalytic activity. The CO oxidation results of Pt-containing samples also reflected the structure and physicochemical properties of  $Pt/TiO<sub>2</sub>$  NPs. The activity of 0.1 Pt/TiO<sub>2</sub>d was similar to that of  $0.5 \, \text{Pt/TiO}_2$ -d because they had similar redox properties ([Fig. 3](#page-4-0)a). The TOF values calculated on the basis of the exposed active sites of Pt NPs (Pt dispersion shown in [Table 1\)](#page-3-1), which implied that the TOF on 0.5 Pt/TiO<sub>2</sub>-d was greater than on 0.1 Pt/TiO<sub>2</sub>-d ([Fig. 4b](#page-4-1)). Pt NPs were supported on the (101) plane of  $TiO<sub>2</sub>$  that exhibited strong interaction, which was beneficial for CO oxidation [[42\]](#page-9-0). Although the increase in the amount of chloroplatinic acid and hydrazine hydrate caused aggregation growth and dispersion decreased of Pt NPs, it was important to enhance the interaction between Pt and TiO<sub>2</sub>. This result could be identified by the  $H_2$ -TPR curves of Pt/TiO<sub>2</sub> nanoparticles after calcination [\(Fig. 3b](#page-4-0)). The enhancement of the

interaction between Pt and  $TiO<sub>2</sub>$  as the Pt content further enhanced the CO oxidation activity and improved the catalytic capability of the single active site. Consequently, the  $0.5 \, \text{Pt/TiO}_2$ -d sample exhibited a greater TOF value. The interaction between Pt and  $TiO<sub>2</sub>$  was further enhanced and the activity was increased with the removal of organics after calcination. Therefore, the  $0.5 \, \text{Pt/TiO}_2$ -c sample exhibits the best CO oxidation performance. The mutual verification of the CO oxidation results and the above characterization data confirmed that Pt NPs have indeed bound to  $TiO<sub>2</sub>$  in the dispersion liquid. The strong interaction between Pt NPs and  $TiO<sub>2</sub>$  is beneficial for catalytic combustion.

## 3.2. Catalytic activity of  $Pt/TiO<sub>2</sub>$  NPs

[Fig. 5a](#page-5-0) shows the catalytic activities of all powder samples for toluene combustion to evaluate the catalytic combustion properties of the fabricated Pt/TiO<sub>2</sub> NPs. The activity of Pt-containing samples was enhanced with the organics removed after calcination, which were consistent with CO oxidation. The  $0.5 \, Pt/TiO<sub>2</sub>$ -d sample exhibited larger TOF values than those of the  $0.1$  Pt/TiO<sub>2</sub>-d sample [\(Fig. 5b](#page-5-0)). The catalytic combustion results showed that the nano-Pt/TiO<sub>2</sub> dispersion liquid with catalytic combustion activity could be successfully prepared by following the strategy in Fig. S1a, which ensured the follow-up preparation of catalytic combustion monolithic catalysts by simply spraying on different substrates.

<span id="page-4-1"></span>

Fig. 4. (a) CO oxidation performance of Pt/TiO<sub>2</sub> nanoparticles. (b) TOF for CO oxidation on 0.1 Pt/TiO<sub>2</sub>-d and 0.5 Pt/TiO<sub>2</sub>-d. Reaction conditions: 1% CO, 21% O<sub>2</sub>, balance N<sub>2</sub>, WHSV = 24,000 mL g<sup>-1</sup> h<sup>-1</sup>.

<span id="page-5-0"></span>

Fig. 5. (a) Toluene catalytic combustion performance of Pt/TiO<sub>2</sub> nanoparticles. (b) TOF for toluene combustion on 0.1 Pt/TiO<sub>2</sub>-d and 0.5 Pt/TiO<sub>2</sub>-d. Reaction conditions: 2000 ppm Toluene, 21% O<sub>2</sub>, balance N<sub>2</sub>, WHSV = 34,000 mL g<sup>-1</sup> h<sup>-1</sup>.

#### 3.3. Properties of  $Pt/TiO<sub>2</sub>$  monolithic catalysts

### 3.3.1. Cordierite honeycomb substrate

The photos and SEM images of  $0.5 \, Pt/TiO<sub>2</sub>$  cordierite monolithic catalysts are shown in [Fig. 6.](#page-5-1) Unlike blank cordierite honeycomb, the cordierite surface was covered with a film after spraying the dispersion liquid. The highly dispersed active NPs could be clearly observed after removing organics by calcination, as shown in the SEM images. The same phenomenon was observed on the SEM images of the as-prepared monolithic catalysts based on reticulated sic, foamed alumina and brick ([Fig. 10](#page-7-0)). The presence of organics in the dispersion liquid will lead to the formation of a Pt/TiO<sub>2</sub> active film after spraying on the substrate surface. The active NPs are dispersed in the film as in the dispersion liquid. The active NPs can be firmly dispersed on the surface when the organics are removed by calcination under the effect of the substrate. Therefore, the spraying of the active NP dispersion liquid, as shown in Fig. S1b, is an effective method for preparing a monolithic catalyst with excellent dispersibility of the active components. The dispersion of active components is an important factor that affects the catalyst performance [43–[45\]](#page-9-1). Generally, the more dispersed the active components, the more active sites are exposed. Thus, the catalytic activity of the catalyst is improved. The monolith catalyst prepared only by simple spraying the active NP dispersion liquid on the substrate can obtain good catalytic performance.

[Fig. 7a](#page-6-0) shows the toluene catalytic combustion activities of the monolithic catalysts prepared by different methods. [Fig. 7b](#page-6-0) shows the temperatures that correspond to 10%, 50%, and 90% toluene conversion ( $T_{10}$ ,  $T_{50}$ , and  $T_{90}$ , respectively). The catalytic activity of the Pt/ TiO<sub>2</sub> cordierite monolithic catalysts prepared by our strategy was superior to the traditional slurry-coating method. In particular, the  $T_{10}$  of the monolithic catalyst prepared by our strategy was significantly lower

than the slurry-coating method. For example, the  $T_{10}$  of 0.5 Pt/TiO<sub>2</sub>/CH was 204 °C, and R-0.5 Pt/TiO<sub>2</sub>/CH reached 222 °C. This phenomenon showed that the cordierite sprayed by the nano- $Pt/TiO<sub>2</sub>$  dispersion liquid had considerable catalytic activity for toluene combustion without further calcination activation. Accordingly, the active NPs dispersion liquid spray method is a simpler and more effective energy-saving method for preparing monolith catalysts than the conventional method.

In addition to the catalytic performance of the monolith catalyst, the adherence of the active component on the substrate is also an important indicator for evaluating the catalyst. Adhesion test was conducted to study the firmness of the active components on the substrate ([Fig. 8](#page-6-1), Figs. S14 and S15). The loss curves of active components in [Fig. 8a](#page-6-1) show that the curve of R-0.5 Pt/TiO<sub>2</sub>/CH-c was steeper, which indicated the better firmness of active components on the substrate of the monolithic catalyst obtained by dispersion-liquid-spraying method. For example, after ultrasonic vibration for 60 min, the mass loss of 0.5 Pt/  $TiO<sub>2</sub>/CH-c$  was only 0.11%, whereas that of R-0.5 Pt/TiO<sub>2</sub>/CH-c was up to 0.64%. Furthermore, the catalysts after ultrasonic vibration were used for toluene catalytic combustion test [\(Fig. 8b](#page-6-1)). R-0.5 Pt/TiO<sub>2</sub>/CH-c showed a significant decrease in activity after ultrasonic vibration, whereas  $0.5 \, \text{Pt/TiO}_2/\text{CH-c}$  was able to maintain excellent activity. These results showed that although the monolithic catalyst prepared by dispersion liquid spraying is simple, the obtained monolithic catalyst shows improved firmness and activity, which is highly favorable for practical applications.

The stability of a catalyst is an important indicator for determining whether the catalyst can be used in practice. Cordierite monolithic catalysts were prepared with  $0.5$  Pt/TiO<sub>2</sub> dispersion liquid stored for 0, 10, 30, 60, and 100 days (Fig. S12a). The toluene catalytic combustion performances over these catalysts are shown in [Figs. 9a](#page-6-2) and S16.  $T_{50}$ was constant similar to that in the NPs (Fig. S12b and S13). Therefore,

<span id="page-5-1"></span>

Fig. 6. The photos and SEM images of  $0.5$  Pt/TiO<sub>2</sub> cordierite monolithic catalysts.

<span id="page-6-0"></span>

Fig. 7. (a) Toluene catalytic combustion performance of 0.5 Pt/TiO<sub>2</sub> cordierite monolithic catalysts prepared by different methods. (b) The T<sub>10</sub>, T<sub>50</sub> and T<sub>90</sub> of toluene combustion over 0.5 Pt/TiO<sub>2</sub> cordierite monolithic catalysts prepared by different methods. Reaction conditions: 2000 ppm Toluene, 21% O<sub>2</sub>, balance N<sub>2</sub>,  $GHSV = 3000 h^{-1}.$ 

<span id="page-6-1"></span>

<span id="page-6-2"></span>Fig. 8. The loss curves (a) and the toluene catalytic combustion  $T_{50}$  (b) of 0.5 Pt/TiO<sub>2</sub> cordierite monolithic catalysts prepared by different methods after ultrasonic vibration. Reaction conditions: 2000 ppm Toluene, 21% O<sub>2</sub>, balance N<sub>2</sub>, GHSV = 3000 h<sup>-1</sup>.



Fig. 9. T<sub>50</sub> of 0.5 Pt/TiO<sub>2</sub>/CH prepared with 0.5 Pt/TiO<sub>2</sub> stored for different time (a) and durability test of 0.5 Pt/TiO<sub>2</sub>/CH (b) for toluene catalytic combustion; Reaction conditions: 2000 ppm Toluene, 21%  $O_2$ , balance N<sub>2</sub>.

the long-time storage of the dispersion liquid did not affect subsequent spraying in preparing the monolithic catalyst. The long-time running stability test of  $0.5$  Pt/TiO<sub>2</sub>/CH was evaluated at 240 °C and GHSV 6000 h<sup>-1</sup>. The result shown in [Fig. 9](#page-6-2)b. Toluene conversion increased with

operation time in the early stage, because calcination could improve the catalytic activity as shown in [Fig. 7.](#page-6-0) Then toluene conversion was maintained at about 50% during a nearly 80 h test. The as-prepared cordierite monolithic catalyst exhibits superior catalytic stability for

<span id="page-7-0"></span>

Fig. 10. The photos and SEM images of  $0.5$  Pt/TiO<sub>2</sub> monolithic catalysts with different substrates.

toluene combustion, which demonstrates the significant practical potential of our strategy.

## 3.3.2. Other substrates

[Figs. 10 and 11](#page-7-0) show the photos, SEM images, and toluene catalytic combustion performance of the monolithic catalysts with different substrates (reticulated SiC, foamed alumina, and brick) to illustrate that the preparation of  $Pt/TiO<sub>2</sub>$  monolithic catalysts using our strategy is facile and flexible. The catalytic combustion activities on these three monolithic catalysts were basically identical [\(Fig. 11\)](#page-8-24). The complete combustion temperature of toluene over each uncalcined monolith catalyst was approximately 265 °C when WSHV was 370,000 mL  $g^{-1}$ (Pt/TiO<sub>2</sub>) h<sup>-1</sup>. The complete combustion temperature over these

monolithic catalysts after calcination was approximately 240 °C. These phenomena strongly suggest that the active phases with relatively stable and good performance were formed in the as-prepared Pt/TiO<sub>2</sub> dispersion liquid and show that the substrate played a good role in supporting and dispersing the active components [\[46](#page-9-2)]. [Fig. 10](#page-7-0) shows that the active components were highly dispersed on the surface of every substrate. Hence, the active site could exhibit the same good catalytic activity on these three inactive substrates. The  $Pt/TiO<sub>2</sub>$ monolith catalysts with good catalytic combustion performance can be facile and flexibly prepared by spraying the dispersion liquid on various substrates. Therefore, this strategy is a universal and efficient method for preparing  $Pt/TiO<sub>2</sub>$  monolith catalysts.

<span id="page-8-24"></span>

Fig. 11. The toluene catalytic combustion performance of  $0.5 \, \text{Pt/TiO}_2$  monolithic catalysts with different substrates (a: unroasted, b: calcined). Reaction conditions: 2000 ppm Toluene, 21% O<sub>2</sub>, balance N<sub>2</sub>, WHSV = 370,000 mL g<sup>-1</sup>(Pt/TiO<sub>2</sub>) h<sup>-1</sup>.

#### 4. Conclusions

Nano-Pt/TiO<sub>2</sub> dispersion liquid with considerable activity was successfully fabricated by hydrolysis and chemical reduction method. TEM,  $N_2$  adsorption-desorption,  $H_2$ -TPR and CO oxidation results show that the Pt/TiO<sub>2</sub> NPs in the dispersion liquid have good structure and redox properties. The TOF values and characterization results imply that the interaction between Pt and TiO<sub>2</sub> is an important factor that affects the catalytic capability of Pt/TiO<sub>2</sub>. In the Pt/TiO<sub>2</sub> dispersion liquid, Pt NPs are supported on the (101) plane of TiO<sub>2</sub> that exhibits strong interaction. Therefore, the as-prepared  $Pt/TiO<sub>2</sub>$  dispersion liquid has good catalytic activity. Various  $Pt/TiO<sub>2</sub>$  monolithic catalysts are successfully prepared by simply spraying Pt/TiO<sub>2</sub> dispersion liquid on different substrates. SEM images show that the  $Pt/TiO<sub>2</sub>$  NPs are highly dispersed on the substrates. Compared with the  $Pt/TiO<sub>2</sub>$  monolithic catalysts prepared by slurry-coating method, those prepared by our strategy exhibit better firmness and toluene catalytic combustion performance. Moreover, the entire preparation process from dispersion liquid to the monolithic catalyst has no waste water discharge. Thus, our strategy does not cause loss of active components and significantly improves the economics of the precious metal catalyst. The preparation can be completed at a low temperature. This strategy meets the concept of energy conservation and emission reduction. Furthermore, the excellent stability of the Pt/TiO<sub>2</sub> dispersion liquid is suitable for long-time storage. The monolithic catalyst also shows superior long-term operating stability, which is favorable for practical application. The information acquired in this study may provide a new idea for the largescale production of waste-gas-treated monolithic catalysts through a simple, friendly, efficient and economic strategy.

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